

Focal Plane Tip-Tilt Sensing for Improved Single-Mode Fiber Coupling using a 3D-printed Microlens-Ring

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ABSTRACT

Modern extreme adaptive optics (ExAO) systems achieving diffraction-limited performance open up new possibilities for instrumentation. Especially important for the fields of spectroscopy and interferometry is that it opens the possibility to couple light into single-mode fibers (SMFs). However, due to their small size, efficient coupling is very sensitive to the quality of the fiber alignment, beam drifts and higher-frequency tip-tilt aberrations caused by telescope mechanics and vibrations. These residual aberrations are not always sensed and corrected by the adaptive optics (AO) system, leading to unacceptable losses. This is particularly severe for the Extremely Large Telescopes, where their huge structure will mean vibrations increase and optimal AO solutions are even more difficult to implement.

We have created a focal plane sensor to correct for residual aberrations by surrounding the SMF with six Multi-mode fibers (MMFs). On each of the MMFs sits a printed freeform lens, making up a six-element microlens ring (MLR) to refract the light into these surrounding MMFs and thus minimizing light loss in the gap between the fiber cores. This means when the beam is near diffraction limited and centered almost all light couples to the SMF. When the beam is misaligned, it couples to the surrounding cores, which are read out by a detector and processed by the Durham Adaptive Optics Real-Time Control (DARC) software driving a tip-tilt mirror. Currently we are aiming to detect and correct only tip-tilt aberrations. However, choosing to surround the central fiber with six sensing locations potentially allows us to investigate higher order correction modes.

Here we present the design and performance our prototype system. This has been designed for use with the iLocator fiber injection system at the Large Binocular Telescope and can easily be scaled to larger telescopes. We present test results from the KOOL laboratory in Heidelberg and initial integration with the iLocator instrument.

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1. INTRODUCTION

In recent years, the development of advanced adaptive optics (AO) systems has opened up new possibilities: ever-improved image quality, a wider field of view (FoV) and greater sky coverage, leading to new discoveries in fields of astronomy from direct imaging of exoplanets¹ to examining the motions of the stars around Sgr A*². In particular the development of extreme adaptive optics (ExAO) has enabled 8-10m class telescopes to achieve diffraction-limited optical performance, where they would otherwise be seeing-limited.³⁻⁵ Whilst the FoV is limited, this enhanced capability has allowed objects to be viewed with far more detail than ever before.

This improvement has also opened new doors in the field of spectroscopy. Conventionally, spectrographs had large entrance apertures, matched to the seeing limit. In the case of fiber fed spectrographs, this meant using multi-mode fibers (MMFs), with core diameters on the order of 100 microns. Due to their large core diameter, the light from the telescope could be efficiently coupled from the telescope, though this formed a large entrance slit to the spectrograph. Due to the instrument scaling laws, the instruments behind had to be appropriately scaled in size.⁶ Using an ExAO system reduces the size of the point-spread function (PSF) to the diffraction limit, which in turn allows the size of the fiber core to be reduced. These fibers are called single-mode fibers (SMFs) and by coupling into their smaller entrance aperture and usually smaller numerical aperture (NA), the spectrographs that are fed with SMFs can not only be reduced in size, while maintaining the same spectral resolution, but are also free of conventional modal noise.⁷ This leads to increased stability and reduced cost for the instrument. Whilst in principle this is an ideal solution, it comes at the cost of increased alignment tolerances. In recent years, there have been several attempts to couple light from large telescope into SMFs, but the coupling efficiency highly depends on initial fiber alignment, as well as long term movement (beam drifts) and higher-frequency tip-tilt motions.⁸ These can originate both from residual atmospheric aberrations or from telescope and instrument flexure and vibrations.

We have developed a fiber based focal plane tip-tilt sensor to compensate for the movements and tip-tilt vibrations. The concept was introduced in 2017⁹ and a modified preliminary design was presented in 2018, as a tip-tilt sensing micro-lens array (MLA).^{10*} The tip-tilt sensor is based upon a fiber bundle consisting of the “science” SMF and six surrounding sensing MMFs. A MLR sits on top of the fiber bundle tip and refracts increasing amounts of light into the corresponding surrounding sensing fibers as the beam gets misaligned. Analysis of the amount of light coupled into these fibers then allows reconstruction of the actual beam position, i.e. the tip-tilt. This device is designed to be retrofitted to any SMF fed spectrograph, but our prototype is specifically designed for the prototype of the iLocator spectrograph⁷ at the Large Binocular Telescope (LBT).

In this work we outline the working principles of the fiber-based tip-tilt sensor and the corresponding application (Sec. 2), as well as its performance in lab conditions (Sec. 3). In Sec. 4 we discuss advantages of this sensor before summarizing and highlighting future work in Sec. 5.

2. DESIGN

2.1 Optical principle

At the focal plane of the telescope, the tip-tilt sensor is formed of a fiber bundle, which consists of one central SMF (Fibercore SM980, $1/e^2$ mode-field diameter (MFD)= $5.8\mu\text{m}$) and six surrounding MMFs (Thorlabs, core size $105\mu\text{m}$, NA=0.22). The central science fiber guides the light from the telescope to the spectrograph. This fiber is taken from the same production batch as the fiber for iLocator, which allows us to match the MFD and therefore increase throughput. The surrounding MMF are fed to the sensing system. As these fibers do not feed the spectrograph we can make use of the larger core diameter MMFs, to allow for better coupling through reduced alignment tolerances. A small fraction of the light is coupled into these fibers even when the PSF is on

* Despite the difference in name, the working principles presented in this work are identical to the ones in Ref. 10. The actual geometry of the lenses has inspired us to rename the 3D printed lens to micro-lens ring (MLR) instead of micro-lens array (MLA), due to design having a central aperture and the overall shape being point symmetric. The fiber arrangement has changed slightly as printing restrictions required the use of MMFs with larger core sizes.

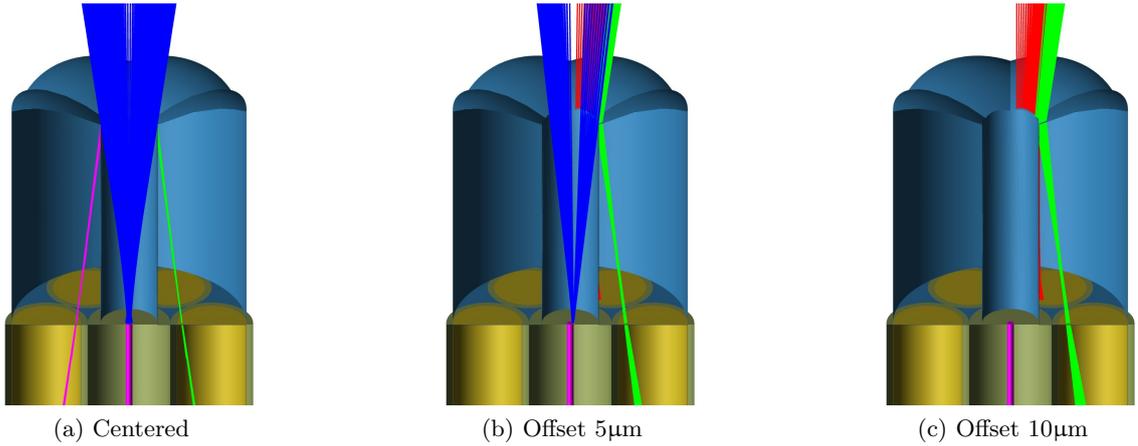


Figure 1. Modeled ray propagation through the micro-lens ring (MLR) for an incoming beam that is (a) aligned and offset by (b) $5\mu\text{m}$ and (c) $10\mu\text{m}$, respectively. In the platescale of iLocator frontend (at $1\mu\text{m}$), the diffraction limit $1.22\lambda/D \sim 60\text{mas}$ corresponds to $\sim 3.9\mu\text{m}$ offset. Please note that the number of rays propagating to the tip of the single-mode fiber (SMF) does not correspond to the coupling efficiency.

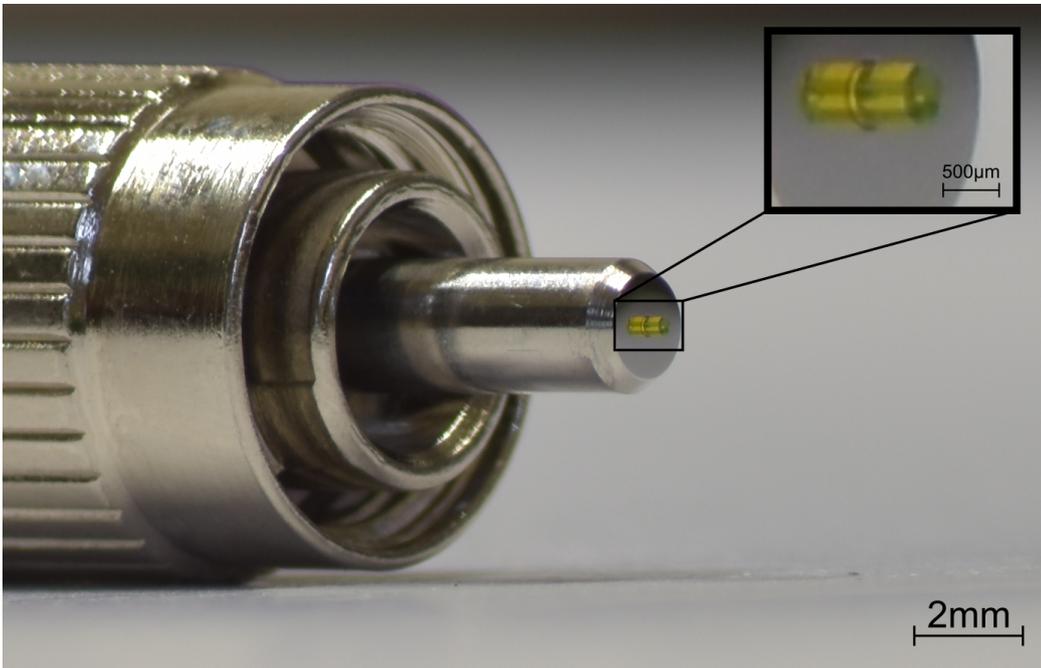


Figure 2. DSLR photograph of micro-lens ring (MLR). The lens stands around $380\mu\text{m}$ tall and around $400\mu\text{m}$ in diameter.

axis to allow for correction feedback. This principle is illustrated in Fig. 1 for an aligned beam (a) that achieves maximum coupling efficiency into the science fiber while only a low amount of light is evenly distributed into the surrounding sensing fibers. When the incoming beam is misaligned by $5\mu\text{m}$ (b) and $10\mu\text{m}$ (c), the amount of light that couples to the sensing fibers located in the direction of the displacement increases.

2.2 Manufacturing

As the design for our MLR is unusual, this would be excessively expensive to design and produce using conventional methods. To make our sensor economically viable we use an in-situ printing technique developed

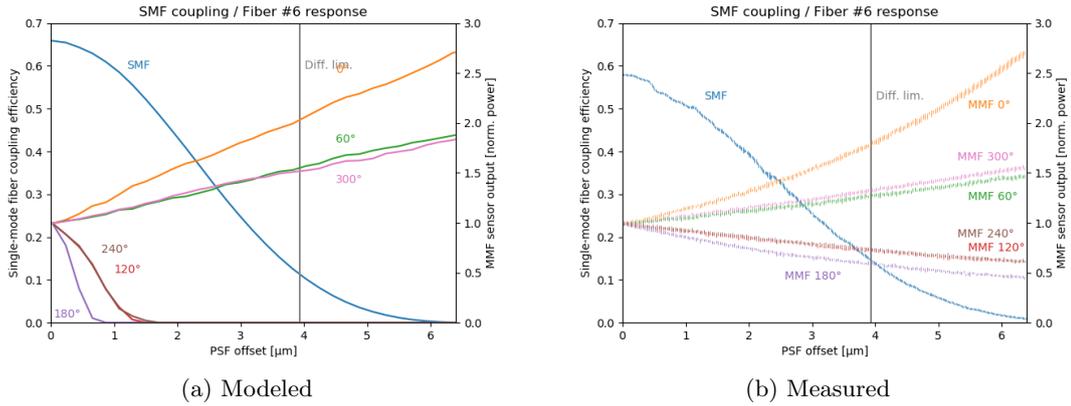


Figure 3. Fiber response in respect to centroid position for both modeled throughput in the ray tracing software *Zemax* (a) and for measured throughput at the iLocator fronted prototype in the lab (b). The vertical gray line denotes the diffraction limit at $\lambda \approx 1\mu\text{m}$. SMF coupling (light blue markers, left y-axis) MMFs coupling (right y-axis) for all six sensing fibers, from same direction as the misalignment (orange marker, corresponding to very right fiber with green rays in Fig. 1), the two adjacent fibers (green, pink, corresponding to second fiber from right with red rays on Fig. 1), to the three fibers on the opposite direction (brown, red, violet, corresponding to two left fibers with pink rays on Fig. 1). All MMFs have differing throughputs, which are normalized in this graph for illustration.

for the telecommunications industry and recently tested for astronomical applications.^{9,11} This technique uses 3D-lithography by two-photon polymerization of a commercial IP-resist from *nanoscribe* and allows us to print directly on the tip of the fiber. Printing on the tip of the fiber allows very precise alignment of the lenses to the cores, as the position of the individual cores is measured before printing and the printing position adjusted to compensate for any differences between design and manufactured bundle.

Fig. 2 shows the completed MLR on top of a FC/PC connector ferrule. The lens stands approximately 380 μm tall and has a diameter of approximately 400 μm . The central aperture has a diameter of approximately 80 μm leaving the light path to the science fiber unaffected. Using an aperture instead of a lens means reflections and surface quality do not play a role in the SMF coupling and the iLocator system does not have to be modified to accommodate the new lens. There is a limited effect due to the edges of this hole vignetting the beam, which results in a slight chromatic coupling efficiency difference.

2.3 Correction

The six surrounding MMFs are separated from the SMF using a 3D printed fiber breakout and rearranged to form a linear array, which is then re-imaged onto a InGaAs camera (First Light C-Red 2). The fluxes of the individual fibers are read, and processed by Durham Adaptive Optics Real-Time Controller (DARC),^{12,13} running on a computer equipped with a consumer grade CPU (i5-8400). DARC then reconstructs the actual centroid position from the six fluxes using a sine-fit approach with some calibration correction. The loop is then closed by an integration correction, feeding a signal to a tip-tilt mirror upstream.

3. RESULTS

Setup and optimization of the fiber-based tip-tilt sensor and the corresponding control system were carried out at the Koenigstuhl Observatory Opto-Mechatronics Laboratory (KOOL),¹⁰ in Heidelberg, Germany. Initial integration tests were conducted at the iLocator frontend prototype at the University of Notre-Dame in Indiana, USA.

Fig. 3 shows the response for the seven individual fibers depending on the centroid position for both modeled throughput in the ray tracing software *Zemax* (a) and for measured throughput at the iLocator fronted prototype in the lab (b). As the incoming beam is de-centered, the SMF coupling (light blue markers, left y-axis) decreases

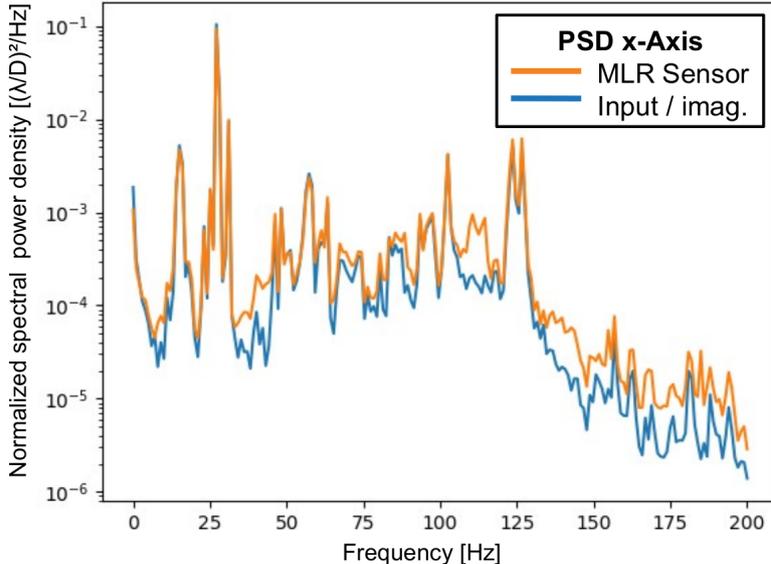


Figure 4. power spectral density (PSD) of the position in x-direction of introduced vibrations as seen on a separate detector that images the PSF (blue) and recovered by the fiber based tip-tilt sensor presented in this work (orange).

significantly within a few μm . On the right y -axis, the response on the sensing fibers is plotted. The amount of coupled light increases for the MMF corresponding to the direction of the offset (orange marker, corresponding to very right fiber with green rays in Fig. 1) as well as the two adjacent fibers (green, pink, corresponding to second fiber from right with red rays on Fig. 1). The throughput of the MMFs opposite to the misalignment decreases (brown, red, violet, corresponding to two left fibers with pink rays on Fig. 1). All MMFs have differing throughputs which are normalized in this graph for illustration. The actual difference originates in residual aberrations in the PSF of the optical setup, in the reconstruction algorithm this is accounted for by a calibration correction.

The overall flux in the six sensing fibers amounts to 2.3% of the overall incoming flux in the lab measurements compared to 10% expected from modeling, which is still being investigated. The SMF coupling efficiency is designed to amount to 67% of the overall incoming light which is less than the $\sim 80\%$ that is theoretically possible when coupling an Airy pattern into a SMF.¹⁴ The measured maximum coupling efficiency is 58% somewhat lower than the expected performance from modeling. This $\sim 10\%$ percentage points difference corresponds to the 70% coupling efficiency into a regular bare SMF that was achieved on the same setup which is also ~ 10 percentage points below the achievable maximum coupling efficiency. We therefore account that difference to residual aberrations in the beam and likely induced in the optics used in generating a simulated telescope beam in laboratory testing.

While most of the modeled and designed characteristics are achieved, these discrepancies in coupling efficiency remain and still need to be fully understood. Furthermore, as seen in Fig. 3b, the response is not as linear as expected. This calls for a more complicated reconstruction algorithm. A simple fitting approach with a sine function was able to recover the measured power spectral density (PSD) quite accurately. This is shown in Fig. 4 for reconstruction (orange) of an artificially introduced vibration (blue). Further calibration correction is being developed to increase accuracy.

4. DISCUSSION

The setup of the correction system and laboratory results show that the fiber based tip-tilt sensor is capable of sensing aberrations. Yet, both coupling efficiency of the SMF at 58% is less than expected (67%) and coupling into the sensing MMFs yields considerably less light than modeled (2.3% compared to 10%). The response also shows a deviation from the predicted linear response, requiring higher order reconstruction algorithms.

When introducing higher order aberrations, the sensor response also shows very characteristic signals. This can already be used to identify signatures of individual modes and will be further improved to yield non-common path (NCP) wavefront data.

Compared to conventional beam stabilization strategies the fiber based tip-tilt sensor presented in this work yields several advantages. While most techniques direct light off to a separate detector such as a quad-cell,¹⁵ the fiber based tip-tilt provides an excellent point of measurement shortly before the focal plane feeding the science fiber. This ensures that there are no NCP aberrations between the science fiber and the sensor, allowing the observer to optimally couple light from the telescope. Furthermore it is very compact and can easily be integrated into any (existing) instrument, only requiring the space for the fiber itself while the read out optics and electronics can be placed in a remote location. This can reduce complexity and cost for different applications. Further research will therefore go into implementing this sensor in small, compact systems and telescopes. Other advantages are the very predictable vignetting of the light within the system and a wide dynamical range as light is coupled into the sensing fibers even for rather large offsets making it also suitable for coarse (initial) alignment processes.

5. CONCLUSION

In this work we present a fiber based tip-tilt sensor that has been designed to improve single-mode fiber (SMF) coupling at the iLocator front end and presented initial laboratory results. Our novel sensor shows a very distinctive response to a misaligned incoming beam. Yet, the coupling efficiencies on both the central science SMF and the surrounding sensing multi-mode fibers (MMFs) are lower than expected. Furthermore, an unexpected non-linearity calls for a more complicated reconstruction algorithm.

The sensor is made possible by new exciting technologies such as the two-photon polymerization used for manufacturing the micro-lens ring (MLR) for this device. Only little light is used for sensing if the beam is aligned and only when the beam becomes misaligned more light is refracted into the sensing fibers. Its advantages are its compact design and sensing at the fiber coupling focal plane, which are not possible with traditional systems, and the potential to sense higher order aberrations. We plan to test it with realistic on-sky conditions at the iLocator front-end at Large Binocular Telescope in the near future. Coupled to a suitable adaptive optics (AO) system, this could be an important tool for coupling SMFs to Extremely Large Telescope (ELT) class telescopes.

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